



Process and Apparatus for the Catalytic Treatment of  
Dust- and Oxygen-Containing Exhaust Gases Containing  
Sulfur Oxides and Nitrogen Oxides

Description

In chemical processes or during the combustion of fossil or secondary fuels - such as garbage or processed garbage - exhaust gases are produced, which apart from other pollutants also contain sulfur oxides and nitrogen oxides. Among experts, the sulfur oxides ( $\text{SO}_2$  and  $\text{SO}_3$ ) are referred to as  $\text{SO}_x$ , and the nitrogen oxides ( $\text{NO}$ ,  $\text{NO}_2$  and  $\text{N}_2\text{O}$ ) are referred to as  $\text{NO}_x$ . Sulfur oxides and nitrogen oxides are gaseous pollutants which act as toxins to the environment and must therefore be removed from the exhaust gases, before the same get into the atmosphere. In the preceding years, considerable efforts were made to reduce the emissions of sulfur oxides and nitrogen oxides. In connection with the denitrification of exhaust gases several processes are being employed. The process most frequently used at present is the SCR process (SCR = Selective Catalytic Reduction). In this process, ammonia or ammonium-containing compounds are introduced into the catalyst-containing reaction chamber, and the nitrogen oxides in the flue gas are reacted to obtain nitrogen and steam. In connection with the SCR process it is reported that in the case of  $\text{SO}_2$ -containing exhaust gases sulfuric acid and ammonium hydrogen sulfate are formed. The formation of sulfuric acid and ammonium hydrogen sulfate is undesired, as in those parts of the plant which are disposed behind the reactor they lead to considerable corrosion problems. In the case of  $\text{SO}_2$ -containing exhaust gases, separate desulfurization plants are therefore generally provided before the SCR process, which desulfurization plants operate according to the principle of the dry or wet flue gas desulfurization plant (REA). In the case of wet processes, the exhaust gas is cooled and reheated for the subsequent SCR process, which is the case in most power plants and garbage incineration plants. Such processes involve high costs, and the formation of  $\text{CaSO}_3$  corresponding to the reaction  $\text{CaO} + \text{SO}_2 \longrightarrow \text{CaSO}_3$  cannot be avoided. The presence of  $\text{CaSO}_3$  in landfill materials is a hazard to the environment.

EP-A-0 671 201 describes a process for separating sulfur trioxide and for denitrification - in particular in garbage incineration plants - ammonia or ammonium-containing compounds being introduced into the flue gas stream before a heat exchanger package, preferably before the last heat exchanger package, or before the flue gas cleaning, so that the catalytic denitrification of the dedusted flue gases is then effected in the low-temperature range, in particular between 100°C and 280°C. The object is to reduce the SO<sub>3</sub> concentration before the SCR reactor by forming ammonium sulfate. The disadvantage of this process consists in that not only ammonium sulfate aerosols are formed, but also ammonium hydrogen sulfate, which later on is precipitated on the catalysts. The ammonium sulfate aerosols can hardly be dedusted in succeeding filter means, so that they represent a considerable burden to the environment. Moreover, a separate gas washer is necessary for the removal of SO<sub>2</sub>. The flue gas must be reheated behind the gas washer, which is not achieved by heat exchange alone. Thus, an additional firing means, e.g. a surface burner with natural gas, is required. Disadvantages include high investment and operating costs.

It is the object underlying the invention to develop a process for the simultaneous desulfurization and denitrification without the formation of ammonium sulfate or ammonium hydrogen sulfate, wherein NO<sub>x</sub> is decomposed to obtain N<sub>2</sub> and H<sub>2</sub>O.

This object is solved in that the treatment of the exhaust gases containing sulfur oxides and nitrogen oxides is performed in a reactor with solid catalysts in the presence of and/or with the addition of one or more substances selected from the group including free oxides, carbonates, hydroxides of calcium, magnesium, sodium and potassium, and that during the treatment the operating conditions of the gas flow in the free reaction space corresponding to the Froude numbers lie in the range of

$$1 \leq 3/4 \cdot \frac{\mu^2}{g \cdot d_k} \cdot \frac{\rho_g}{\rho_k - \rho_g} \leq 100 \quad \text{with} \quad \frac{\mu^2}{g \cdot d_k} = Fr^2$$

in which:

$\mu$  = the relative gas speed in m/s

Fr = the Froude number

$g$  = the gravitational constant in  $\text{m/s}^2$

Furthermore, costs are preferably minimized by the treatment in the presence of and/or with the addition of one or more substances selected from the group including free oxides, carbonates, hydroxides of calcium, as calcium compounds are more economic as compared to alkali compounds.

As reducing agent,  $\text{NH}_3$ -releasing compounds such as  $(\text{NH}_4)_2\text{SO}_4$ ,  $(\text{NH}_4)_2\text{CO}_3$ ,  $(\text{NH}_4)\text{HCO}_3$ ,  $(\text{COONH}_3)_2\text{H}_2\text{O}$ ,  $\text{HCOONH}_4$ ,  $\text{NH}_3$ ,  $\text{NH}_4\text{OH}$ ,  $\text{H}_2\text{O}-\text{CO}-\text{NH}_2$ ,  $\text{NH}_2\text{CN}$ ,  $\text{Ca}(\text{CN})_2$ ,  $\text{NaOCN}$ ,  $\text{C}_2\text{H}_4\text{N}_4$ ,  $\text{C}_3\text{H}_6\text{N}_6$  and  $\text{NH}_3$ -containing waste waters from photo-chemical plants, singly or several of them, are introduced into the flue gas stream at several points in the gaseous, liquid or solid condition at temperatures in the range between 20000 and 1000°C before entering the catalytic reactor.

A preferred aspect consists in that as reducing agent  $\text{NH}_3$ -releasing compounds in the form of dilute aqueous solutions are introduced into the flue gas stream, preferably at temperatures in the range between 300°C and 550°C. The partial steam pressure in the reaction space is increased and thus the improvement of the incorporation of sulfur is achieved.

A particularly preferred aspect of the invention is the presence or addition of one or more substances selected from the group including free oxides, carbonates, hydroxides of calcium, magnesium, sodium and potassium to the flue gas stream before the addition of  $\text{NH}_3$ -releasing compounds. The formation of ammonium hydrogen sulfate, ammonium sulfate and sulfuric acid is suppressed completely.

Flow to the reactor can be effected from above or from below. A particularly preferred aspect of the invention consists in that the flow to the reactor equipped with the catalysts can alternately be effected from above and from below. By means of this alternate flow, the reactor can easily be kept clean of dust-laden exhaust gases, and blockage of the passages by dust can be avoided. Furthermore, the service life of the catalysts can be increased by alternating the flow to the reactor.

Another preferred aspect of the invention consists in that beside the breakdown of sulfur oxide and nitrogen oxide, the reactor equipped with catalyst can at the same time be used for the breakdown of halogen compounds, halogenated organic compounds, hydrocarbons and CO.

A preferred aspect of the invention consists in that the reactor equipped with catalyst can be used for the breakdown of sulfur oxides and nitrogen oxides in dust-laden exhaust gases in the chemical and metallurgical industries as well as in the cement and lime industries, in power plants and in garbage incineration plants in

the process flow at temperatures in the range between 200°C and 500°C without additional preheating of the exhaust gas.

Another aspect in accordance with the invention is the apparatus for the treatment of exhaust gas containing dust and oxygen. The drawings represent examples of the apparatus for performing the process, which are explained in detail below. In the drawings:

Fig. 1 schematically shows an arrangement of the apparatus in the cement industry;

Fig. 2 schematically shows an apparatus for the cement industry;

Fig. 3 schematically shows an arrangement of the apparatus for power plants;

Fig. 4 schematically shows an apparatus for power plants.

Fig. 1 shows the arrangement of the inventive apparatus in a cement factory with rotary kiln 16 for the production of clinker. The SCR reactor 19 with catalyst modules 20 and dust blowers 18 is arranged in flow direction behind the suspension-type cyclone heat exchanger 13 comprising the cyclones Z1 to Z4 which are connected with each other. For metering  $\text{NH}_3$ -releasing compounds, a plurality of points A, B, C, D and E are provided at temperatures in the range from 300°C to 1000°C. For metering ammonia, ammonia solution or urea solution, the metering points A, B and C are preferred. For metering  $\text{NH}_3$ -containing waste water from phototechnical plants and other compounds of  $\text{NH}_3$ , the metering points D and E are preferably used. The calcium-containing raw meal 12 is charged between the cyclones Z1 and Z2. After the treatment in the SCR reactor 19, the exhaust gas is either supplied to the chimney 24 via the raw material grinder 21 and the dedusting means 23 in the case of a combined operation, or is supplied to the chimney 24 via the evaporative cooler 22 and the dedusting means 23 in the case of a direct operation.

Fig. 2 shows an apparatus with gas conduit from the bottom to the top, from the top to the bottom and alternately from below and from above.

For an alternate gas conduit from below and from above in operation, some additional lines and flaps are provided, which are shown in Fig. 2. When alternately switching the exhaust gases from the bottom to the top, calcium-containing compounds and  $\text{NH}_3$ -containing exhaust gas are introduced into the reactor 19 from below via line F and are withdrawn via line G. The flaps M1, M4, M6 and M8 remain closed, and the flaps M2, M3, M5 and M7 remain open. In the case of a combined operation, the exhaust gas is then passed via the WT blower 25 and line H to the raw material grinder 21 and the dedusting means 23 to the chimney 24, or in the case of a direct operation via line I to the evaporative cooler 22 and the dedusting means 23 to the chimney 24. The flaps M9 and M10 mutually act to block the combined operation or the direct operation. When alternately switching the gas conduit from above, calcium compounds and  $\text{NH}_3$ -containing exhaust gas are introduced into the SCR reactor 19 from above via lines J and G behind the cyclone heat exchanger 13, and are discharged from below via lines F and K to the WT blower 25. The flaps M1, M8, M5, M3, M4 and M6 remain open, and the flaps M2 and M7 remain closed. In the case of a combined operation, the exhaust gas is then passed through the WT blower 25 via line H to the raw material grinder 21 and the dedusting means 23 to the chimney 24, or in the case of a direct operation via line I to the evaporative cooler 22 and the dedusting means 23 to the chimney 24.

In the case of an accident or shut-down of the SCR reactor 19, the addition of  $\text{NH}_3$ -releasing compounds is stopped and discharged via a bypass, i.e. via line K through the WT blower 25 either to the raw material grinder 21 or to the evaporative cooler 22. The flaps M2, M4, M6 remain open and the flaps M3, M1, M8, M7 and M5 remain closed. The cold-air flap M11 is provided to control the exhaust gas temperature before the SCR reactor 19.

In the case of a design with gas conduit only from below, line J and the flaps M1, M8 and M7 are superfluous and thus the apparatus is only provided with an SCR reactor 19, bypass line K and the flaps M3, M4, M5, M6. In connection with space and cost savings, two individual flaps may be equipped with a switching flap. In addition, the WT blower 25 may be installed shortly behind the cyclone heat exchanger 13, depending on space requirements and design.



dust content =  $8000 \text{ mg/m}^3_{\text{N tr}}$

$\text{O}_2$  content = 3.2 vol-%

Temperature in the reactor =  $320^\circ\text{C}$

The density of the gas is calculated with reference to the gas composition. The dust content before entrance into the reactor (chiefly  $\text{CaO}$  and  $\text{Ca(OH)}_2$ ) is  $8000 \text{ mg/m}^3_{\text{N tr}}$ . The determined particle density of the dust is about  $3.1 \text{ kg/m}^3$ . With reference to these data and operating conditions, a gas speed of  $6.5 \text{ m/s}$  is determined corresponding to the Froude numbers.

In the experiments, there were used honeycomb catalysts with different contents of active components and with the following specifications:

free opening surface = 85 %

pitch = 11 mm

clear width of the passages = 10 mm

wall thickness = 1 mm.

The content of active component (e.g.  $\text{V}_2\text{O}_5$ ) in the catalysts is 0.1 %, 0.3 %, 1 %, 3 % and 5 %. As reducing agent, gaseous  $\text{NH}_3$  with a stoichiometry, i.e. a molar ratio  $\text{NH}_3/\text{NO}_x$  of 0.85 is added before entry in the reactor.

For the experiments, a steel grid made of stainless steel is mounted on the module of the catalyst as a protection against wear before entry of the dust-laden exhaust gas.

The gas components  $\text{NO}_x$ ,  $\text{SO}_x$ ,  $\text{NH}_3$ ,  $\text{CO}$ ,  $\text{CO}_2$  and  $\text{H}_2\text{O}$  are measured continuously before and behind the reactor by means of a multicomponent analyzer MCS-100.

The breakdown of the most important components in dependence on the content of active component  $\text{V}_2\text{O}_5$  is represented in the following Table:



Active component of the catalyst	Breakdown of NO <sub>x</sub>	Breakdown of SO <sub>x</sub>	Breakdown of hydrocarbons
V <sub>2</sub> O <sub>5</sub> content 0.1 %	34	3	10
V <sub>2</sub> O <sub>5</sub> content 0.3 %	42	5	15
V <sub>2</sub> O <sub>5</sub> content 1.0 %	56	22	30
V <sub>2</sub> O <sub>5</sub> content 3.0 %	75	70	55
V <sub>2</sub> O <sub>5</sub> content 5.0 %	95	90	70

The results show that with the inventive process NO<sub>x</sub> and SO<sub>x</sub> are decomposed when suitable operating conditions - gas flow and selection of the active components - are adjusted.

In the experiments with 5 % V<sub>2</sub>O<sub>5</sub>, the NH<sub>3</sub> content of the exhaust gas is about < 1 mg/m<sup>3</sup><sub>N.tr.</sub>. The analyses of the dust behind the catalyst exhibit no formation of ammonium sulfate, ammonium hydrogen sulfate or CaSO<sub>3</sub>. The SO<sub>x</sub> content is bound as CaSO<sub>4</sub>. Moreover, these experiments exhibit not dust deposits in the reactor or in the catalyst passages.

In another series of experiments, the operating conditions of the gas flow in the free reaction space are changed outside the inventive Froude numbers with the same gas composition, the same dust content and the same catalysts. It is noted that at gas speeds below 4 m/s the breakdown of NO<sub>x</sub> decreased considerably and the differential pressure at the reactor 19 increased. The result is a complete blockage of the catalyst passages with dust.